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ABSTRACT (maximum 100 words)  
Silver is evaporated into an inert gas flowing at pressures between 0.1 and 3 torr and nucleates to form clusters in a size range of 40 to 110 Å. This two-phase mixture flows through a two stage molecular beam into a modified electron microscope. Electron diffraction patterns are taken in the cluster beam and analyzed assuming the bulk, face centered cubic unit cell and using a thirteen-beam, multislice, multiple scattering program. Deviations from the bulk structure are seen and are larger for smaller cluster size. Several possible interpretations are discussed. The use of inert

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20. Molecular gasses as carriers is found to greatly increase cluster production.

PRODUCTION AND ELECTRON DIFFRACTION STUDIES  
OF SILVER METAL CLUSTERS IN THE GAS PHASE

by

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ABSTRACT

Silver is evaporated into an inert gas flowing at pressures between 0.1 and 3 torr and nucleates to form clusters in a size range of 40 to 110 Å. This two-phase mixture flows through a two stage molecular beam into a modified electron microscope. Electron diffraction patterns are taken in the cluster beam and analyzed assuming the bulk, face centered cubic unit cell and using a thirteen-beam, multislice, multiple scattering program. Deviations from the bulk structure are seen and are larger for smaller cluster size. Several possible interpretations are discussed. The use of inert molecular gasses as carriers is found to greatly increase cluster production.

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KONTRAKTOR

The objective of this study was to obtain information on the structure of small clusters of metal atoms, prepared by evaporation into a low pressure inert gas, by analysis of their electron diffraction patterns. Potentially large effects of supporting substrates upon the clusters' structures were avoided by employing the quenching gas as a carrier to transport the clusters through a differentially pumped gaseodynamic system (forming a "molecular" beam) into a high vacuum region where the electron diffraction pattern can be recorded<sup>(1)</sup>. A necessary subsidiary goal was to discover conditions which produce sufficiently dense metal cluster beams so that electron diffraction patterns can be observed.

EXPERIMENTAL

The metal cluster generator has been described previously<sup>(1)</sup> and is schematically illustrated in Fig. 1. This open cluster source has been mounted in one port of the "diffraction chamber" of an Hitachi HU-11A/B, operated as an electron beam source (condenser lenses only used). The electron microscope has been modified with the addition of a coarse aperture just above the cluster source and additional pumping capacity of 1,000 l/sec. Electron diffraction patterns are recorded on silver photographic plates.

The metal vapor source used was a small helix, hand-wound from tungsten wire (0.38 mm diameter) into which one or more small ingots formed from 99.999% silver, are inserted. The amount of silver in each charge is estimated to be in the range 0.1 - 0.25 g. The gas

inlet tubing was shortened so that it now discharges from behind the heater rather than between heater and  $N_1$ , as shown in Fig. 1. Pressures measured at various points, with gas flow on but oven power off, are recorded in Table I. Except for the lowest pressure with helium, which is outside the range of operating conditions actually used, the pressure ratios are low enough to cause "choked", sonic, constant mass flow rates through both  $N_1$  and  $N_2$ . However, due to the pressure drop through the inlet gas tube, this flow is everywhere subsonic.

The flow transit time for a monotonic gas is calculated to be ca. 0.5 sec for the open chamber. One-fifth to one-eighth of the carrier gas exits via  $N_2$ . A somewhat higher proportion of the metal clusters ought to pass through  $N_2$  and the electron beam, because of their much greater "molecular" weight ( $k \times 10^4$  to  $2 \times 10^6$ ).

Diffraction patterns, if observed at all, are commonly visible for only 10 seconds, and never for more than about 90 seconds. We were clearly not operating the oven under steady-state conditions, although they were constant over the plate exposure time (a fraction of a second). The oven gas pressure and temperature,  $P_0$  and  $T_0$ , along with other experimental information, are summarised in Table II.

Exposed plates were developed in the usual manner and their degree of blackening quantified by scanning across a diameter of the diffraction pattern with a recording microdensitometer. Patterns from three plates

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are presented in Fig. 2. Peak spacings (diffraction ring diameters), peak widths, and peak heights are all measured from these densitometer records. Calibration of spacings and minimum peak widths was obtained by tracing the patterns obtained from a commercial aluminum diffraction standard. Unit cell dimensions were derived from ring radii using the expression:

$$a = L_2 \sqrt{h^2 + k^2 + l^2 / (r_1 - 3r^2/8L^2)} \quad (1)$$

where  $L_2$  is a "Womers constant" determined from the aluminum standard,  $r_1 = 0.053551$  & for the 50 Kev electrons, and  $L = 47.13$  cm. The term in  $(r/L)^2$  is a small flat-plate correction. Cluster diameters,  $D$ , were estimated from peak widths using

$$D = L_2 / \sqrt{w^2 - w_0^2} \quad (2)$$

where  $w$  is the observed peak width and  $w_0$  is the "instrument broadening" taken to be the peak width found for the aluminum standard. Peak heights were taken to be proportional to the diffracted power in each peak and were corrected for the non-linear response of the plates. Estimated standard deviations were assigned to each intensity,  $\sigma_{\text{obs}}$ , and multiplied by the same correction factors. It should be emphasized that only diffraction patterns strong enough to be seen by eye on the phosphor screen were recorded.

#### RESULTS AND DISCUSSION

##### Source performance

In addition to varying gas pressures and filament temperatures, in search of optimum conditions for the production of high densities of small clusters, we also explored the effect of changing the carrier

gas. Argon and helium show differences reflecting their differing atomic masses and collision cross sections (2, 3). Past experience with nucleation studies indicates that a larger number of smaller clusters should result from a more rapid cooling of the hot metal vapor (1).

The chemically inert molecular gas, sulfur hexafluoride SF<sub>6</sub>, with its many internal degrees of freedom, i.e., its much larger heat capacity per molecule, should be a more effective third body in the early stages of cluster formation. Since silver has a relatively small affinity for oxygen, CO<sub>2</sub> was also successfully used as a carrier gas.

Greatly increased production of silver clusters was observed using molecular gases. This occurred at substantially lower filament temperatures (i.e., lower vapor pressures) as indicated in Table II. Silver deposits on the oven liner were collected on microscope grids. Electron diffraction patterns from samples showed metallic silver only, with no evidence for chemical reaction with the molecular gasses.

An argument was made in an earlier paper (1) for a relationship between cluster size and the product of oven pressure,  $P_0$ , times the temperature of the evaporating metal sample,  $T_{\text{ov}}$ . The earlier study used the same cluster generator and used one carrier gas (Ar) and several metals (In, Bi, and Pb), while this work is for one metal (Ag) and several carrier gases (Ar, He, CO<sub>2</sub>, and SF<sub>6</sub>). Both sets of observations are displayed in Fig. 3. All the results with the filament source are consistent, the heavier gases producing a given cluster size at lower  $P_0 T_{\text{ov}}$ .

#### Diffraction Analysis

From the diffraction patterns, one easily obtains crystalline unit cell dimensions and crystallite sizes from the diffracted rings'. However, more detailed atomic scale diameters and breadths, respectively. However, more detailed atomic scale information is contained in the relative intensities of the rings. This information may be extracted by matching the intensities calculated from a model to the observed intensities. However, the calculations leading from model to diffracted intensities are more complex in the case of electron scattering than for X-rays or neutrons because of multiple scattering or "dynamical" effects. These effects are large enough to cast doubt upon any such analysis based upon simpler kinematic (or the first-approximation, Blackmann-formula (1)) calculations (5).

Accordingly, a computer program has been written which calculates the diffracted intensities in as accurate an approximation as the available resources would permit. This program calculates the intensities of "systematically-related" sets of (from 5 to 13) diffracted beams using a Shirley-type matrix(6) in a multisllice method (7) and includes the effects of absorption (8). Intensities integrated over all orientations are obtained by summing the results of repeated calculations and the values for a succession of slab thicknesses stored. These infinite-slab results are converted to those for spherical particles by taking appropriately weighted averages. An example is shown in Fig. 4, normalised to the (311) reflection. If the scattering were kinematical the curves would all be horizontal from their values at  $D_t = 0$ . Variations from (311) (also varying) by a factor of 2 to 3 can be seen at large  $D_t$ .

The corrected peak-height data obtained from the plates are used as input to the computer program which performs a simple search procedure to find the best-fitting value of the root mean square amplitude of thermal motion,  $U$ . At every search step the best-fitting scale factor,  $k$ , and cluster diameter,  $D_t$ , are also found. The function minimised is:

$$R_K = \left[ \sum (I_{\text{obs}} - k I_{\text{calc}})^2 / \sigma_{\text{obs}}^2 \right]^{1/2} / \left[ \sum (I_{\text{obs}} / \sigma_{\text{obs}})^2 \right]^{1/2}$$

The resulting values of  $D_t$ ,  $U$ , and  $R_K$  are reported in Table II. The  $R_K$  values are calculated as for  $R_M$ , but with "kinematic"  $I_{\text{calc}}$  and the same  $U$ . In every case  $R_K$  is seen to be an improvement over  $R_M$  but they are still a good deal larger than the quality of the data would lead us to expect. In addition, if this model and calculation are to be deemed successful, strong correlations between several of the quantities in Table II should be seen. For example, at a given cluster size,  $U$ , and the cell dimension,  $a$ , should increase together (indicating higher temperature clusters) and  $D_t$  and  $D_c$  should agree. A strong indication of the reason for this failure to agree is seen in Figure 5 which shows worsening agreement between observed and calculated intensities with decreasing cluster size. This indicates that the bulk fcc structure is not maintained at small cluster sizes. Further support for this view is found in the consistent pattern of deviations displayed in Figure 6. The most prominent features, (111) observed too strong and (100) too weak, have also been reported for clusters of lead(5) and of argon.(9)

A variety of models, other than the bulk fcc structure, have been considered but all have one or more qualitative features that do not fit the observations. These include the combined fcc plus liquid model (5), stacking faults and twinning between fcc regions, decahedral (pentagonal bipyramidal) and icosahedral sphere packing models (10), and a "liquid-like" distribution of vacancies in an fcc matrix. It is reasonable to suppose that a partially liquid or amorphous or "polytetrahedral" structure is correct, but this has not been demonstrated. Single-phase (homogeneous) models other than fcc can be tested with the multi-beam computer program by replacing one subroutine.

#### ACKNOWLEDGMENTS

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TABLE I  
Oven Operating Pressures a)

| Gas | Inlet <sup>b)</sup><br>$P_{\text{in}}$<br>torr | Oven Conditions |                | Diffraction Information |                  | Plates No. | Cartier<br>gas | Oven<br>gas | Wedges<br>X | X    | $\frac{\lambda}{\lambda'}$ | $\frac{P_0}{P_0'}$ | $\frac{P_0}{P_0''}$ | $\frac{P_0}{P_0''''}$ | $\frac{P_0}{P_0'''} \cdot \frac{P_0}{P_0''}$ | $\frac{P_0}{P_0'''} \cdot \frac{P_0}{P_0''} \cdot \frac{P_0}{P_0''''}$ |
|-----|--|-----------------|----------------|-------------------------|------------------|------------|----------------|-------------|-------------|------|----------------------------|--------------------|---------------------|-----------------------|--|--|
|     |  | $P_0$<br>torr   | $P_0'$<br>torr | $P_0''$<br>torr         | $P_0'''$<br>torr |            |                |             |             |      |                            |                    |                     |                       |  |  |
| He  | 1.28   | 625             | 55             | 1500                    | 4.078            | 43         | 37             | 0.33(5)     | 10.2        | 18.0 |                            |                    |                     |                       |  |  |
| 6   | He   | 1.28            | 625            | 55                      | 1500             | 4.078      | 43             | 37          | 0.33(5)     | 10.2 | 18.0                       |                    |                     |                       |  |  |
| 7   | He   | 1.28            | 625            | 55                      | 1500             | 4.079      | 36             | —           | —           | —    | —                          |                    |                     |                       |  |  |
| 13  | He   | 2.90            | 530            | 100                     | 1300             | 4.058      | 56             | 37          | 0.08(12)    | 34.9 | 22.3                       |                    |                     |                       |  |  |
| 14  | He   | 2.90            | 530            | 100                     | 1300             | 4.059      | 60             | 50          | 0.09(4)     | 15.2 | 24.7                       |                    |                     |                       |  |  |
| 25  | Ar   | 2.90            | 530            | 100                     | 1300             | 4.059      | 74             | —           | —           | —    | —                          |                    |                     |                       |  |  |
| 160 | Ar   | 3.2             | 545            | 140                     | 1500             | 4.066      | 53             | 42          | 0.18(3)     | 16.6 | 24.2                       |                    |                     |                       |  |  |
| 8   | Ar   | 0.51            | 770            | 50                      | 2300             | 4.085      | 72             | —           | —           | —    | —                          |                    |                     |                       |  |  |
| 9   | Ar   | 0.51            | 770            | 50                      | 2300             | 4.085      | 72             | —           | —           | —    | —                          |                    |                     |                       |  |  |
| 10  | Ar   | 0.60            | 760            | 50                      | 2300             | 4.085      | 72             | —           | —           | —    | —                          |                    |                     |                       |  |  |
| 3   | N <sub>2</sub>                                 | 1.54            | 695            | 45                      | —                | 4.095      | 68             | —           | —           | —    | —                          |                    |                     |                       |  |  |
| 4   | N <sub>2</sub>                                 | 1.54            | 695            | 50                      | —                | 4.095      | 69             | 7           | 0.15(2)     | 6.2  | 9.3                        |                    |                     |                       |  |  |
| 39  | CO <sub>2</sub>                                | 0.27            | 625            | 20                      | 1100             | 4.080      | 46             | —           | —           | —    | —                          |                    |                     |                       |  |  |
| 40  | CO <sub>2</sub>                                | 0.27            | 625            | 20                      | 1100             | 4.080      | 46             | —           | —           | —    | —                          |                    |                     |                       |  |  |
| 30  | CO <sub>2</sub>                                | 0.55            | 720            | —                       | —                | 4.090      | 30             | 60          | 0.25(6)     | 32.0 | 39.0                       |                    |                     |                       |  |  |
| 36  | CO <sub>2</sub>                                | 0.31            | 620            | 1                       | 1100             | 4.063      | 50             | 10          | 0.27(4)     | 18.1 | 21.9                       |                    |                     |                       |  |  |
| 34  | CO <sub>2</sub>                                | 0.37            | 600            | 25                      | 1100             | 4.076      | 63             | —           | —           | —    | —                          |                    |                     |                       |  |  |
| 35  | CO <sub>2</sub>                                | 0.36            | 620            | 30                      | 1100             | 4.076      | 57             | —           | —           | —    | —                          |                    |                     |                       |  |  |
| 33  | CO <sub>2</sub>                                | 0.36            | 620            | 20                      | 1100             | 4.075      | 66             | 180         | 0.20(7)     | 12.0 | 22.6                       |                    |                     |                       |  |  |
| 22  | CO <sub>2</sub>                                | 0.73            | 625            | 30                      | 1100             | 4.065      | 110            | 100         | 0.20(3)     | 8.7  | 21.4                       |                    |                     |                       |  |  |

TABLE II

SUMMARY OF EXPERIMENTS AND THEORETICAL COMPARISONS  
(SLIVER CLUSTERS IN VARIOUS CARTIER GASES)

| Experiment No. | Cartier<br>gas | Oven Conditions |                | Diffraction Information |                  | Plates No. | Cartier<br>gas | Oven<br>gas | Wedges<br>X | X    | $\frac{\lambda}{\lambda'}$ | $\frac{P_0}{P_0'}$ | $\frac{P_0}{P_0''}$ | $\frac{P_0}{P_0''''}$ | $\frac{P_0}{P_0'''} \cdot \frac{P_0}{P_0''}$ | $\frac{P_0}{P_0'''} \cdot \frac{P_0}{P_0''} \cdot \frac{P_0}{P_0''''}$ |
|----------------|----------------|-----------------|----------------|-------------------------|------------------|------------|----------------|-------------|-------------|------|----------------------------|--------------------|---------------------|-----------------------|--|--|
|                |                | $P_0$<br>torr   | $P_0'$<br>torr | $P_0''$<br>torr         | $P_0'''$<br>torr |            |                |             |             |      |                            |                    |                     |                       |  |  |
| a)             | He             | 1.28            | 625            | 55                      | 1500             | 4.078      | 43             | 37          | 0.33(5)     | 10.2 | 18.0                       |                    |                     |                       |  |  |
| b)             | He             | 1.28            | 625            | 55                      | 1500             | 4.078      | 43             | 37          | 0.33(5)     | 10.2 | 18.0                       |                    |                     |                       |  |  |
| c)             | He             | 1.28            | 625            | 55                      | 1500             | 4.078      | 43             | 37          | 0.33(5)     | 10.2 | 18.0                       |                    |                     |                       |  |  |
| d)             | He             | 1.28            | 625            | 55                      | 1500             | 4.078      | 43             | 37          | 0.33(5)     | 10.2 | 18.0                       |                    |                     |                       |  |  |
| e)             | He             | 1.28            | 625            | 55                      | 1500             | 4.078      | 43             | 37          | 0.33(5)     | 10.2 | 18.0                       |                    |                     |                       |  |  |
| f)             | He             | 1.28            | 625            | 55                      | 1500             | 4.078      | 43             | 37          | 0.33(5)     | 10.2 | 18.0                       |                    |                     |                       |  |  |
| g)             | He             | 1.28            | 625            | 55                      | 1500             | 4.078      | 43             | 37          | 0.33(5)     | 10.2 | 18.0                       |                    |                     |                       |  |  |
| h)             | He             | 1.28            | 625            | 55                      | 1500             | 4.078      | 43             | 37          | 0.33(5)     | 10.2 | 18.0                       |                    |                     |                       |  |  |
| i)             | He             | 1.28            | 625            | 55                      | 1500             | 4.078      | 43             | 37          | 0.33(5)     | 10.2 | 18.0                       |                    |                     |                       |  |  |
| j)             | He             | 1.28            | 625            | 55                      | 1500             | 4.078      | 43             | 37          | 0.33(5)     | 10.2 | 18.0                       |                    |                     |                       |  |  |
| k)             | He             | 1.28            | 625            | 55                      | 1500             | 4.078      | 43             | 37          | 0.33(5)     | 10.2 | 18.0                       |                    |                     |                       |  |  |
| l)             | He             | 1.28            | 625            | 55                      | 1500             | 4.078      | 43             | 37          | 0.33(5)     | 10.2 | 18.0                       |                    |                     |                       |  |  |
| m)             | He             | 1.28            | 625            | 55                      | 1500             | 4.078      | 43             | 37          | 0.33(5)     | 10.2 | 18.0                       |                    |                     |                       |  |  |
| n)             | He             | 1.28            | 625            | 55                      | 1500             | 4.078      | 43             | 37          | 0.33(5)     | 10.2 | 18.0                       |                    |                     |                       |  |  |
| o)             | He             | 1.28            | 625            | 55                      | 1500             | 4.078      | 43             | 37          | 0.33(5)     | 10.2 | 18.0                       |                    |                     |                       |  |  |
| p)             | He             | 1.28            | 625            | 55                      | 1500             | 4.078      | 43             | 37          | 0.33(5)     | 10.2 | 18.0                       |                    |                     |                       |  |  |
| q)             | He             | 1.28            | 625            | 55                      | 1500             | 4.078      | 43             | 37          | 0.33(5)     | 10.2 | 18.0                       |                    |                     |                       |  |  |
| r)             | He             | 1.28            | 625            | 55                      | 1500             | 4.078      | 43             | 37          | 0.33(5)     | 10.2 | 18.0                       |                    |                     |                       |  |  |
| s)             | He             | 1.28            | 625            | 55                      | 1500             | 4.078      | 43             | 37          | 0.33(5)     | 10.2 | 18.0                       |                    |                     |                       |  |  |
| t)             | He             | 1.28            | 625            | 55                      | 1500             | 4.078      | 43             | 37          | 0.33(5)     | 10.2 | 18.0                       |                    |                     |                       |  |  |
| u)             | He             | 1.28            | 625            | 55                      | 1500             | 4.078      | 43             | 37          | 0.33(5)     | 10.2 | 18.0                       |                    |                     |                       |  |  |
| v)             | He             | 1.28            | 625            | 55                      | 1500             | 4.078      | 43             | 37          | 0.33(5)     | 10.2 | 18.0                       |                    |                     |                       |  |  |
| w)             | He             | 1.28            | 625            | 55                      | 1500             | 4.078      | 43             | 37          | 0.33(5)     | 10.2 | 18.0                       |                    |                     |                       |  |  |
| x)             | He             | 1.28            | 625            | 55                      | 1500             | 4.078      | 43             | 37          | 0.33(5)     | 10.2 | 18.0                       |                    |                     |                       |  |  |
| y)             | He             | 1.28            | 625            | 55                      | 1500             | 4.078      | 43             | 37          | 0.33(5)     | 10.2 | 18.0                       |                    |                     |                       |  |  |
| z)             | He             | 1.28            | 625            | 55                      | 1500             | 4.078      | 43             | 37          | 0.33(5)     | 10.2 | 18.0                       |                    |                     |                       |  |  |
| aa)            | He             | 1.28            | 625            | 55                      | 1500             | 4.078      | 43             | 37          | 0.33(5)     | 10.2 | 18.0                       |                    |                     |                       |  |  |
| bb)            | He             | 1.28            | 625            | 55                      | 1500             | 4.078      | 43             | 37          | 0.33(5)     | 10.2 | 18.0                       |                    |                     |                       |  |  |
| cc)            | He             | 1.28            | 625            | 55                      | 1500             | 4.078      | 43             | 37          | 0.33(5)     | 10.2 | 18.0                       |                    |                     |                       |  |  |
| dd)            | He             | 1.28            | 625            | 55                      | 1500             | 4.078      | 43             | 37          | 0.33(5)     | 10.2 | 18.0                       |                    |                     |                       |  |  |
| ee)            | He             | 1.28            | 625            | 55                      | 1500             | 4.078      | 43             | 37          | 0.33(5)     | 10.2 | 18.0                       |                    |                     |                       |  |  |
| ff)            | He             | 1.28            | 625            | 55                      | 1500             | 4.078      | 43             | 37          | 0.33(5)     | 10.2 | 18.0                       |                    |                     |                       |  |  |
| gg)            | He             | 1.28            | 625            | 55                      | 1500             | 4.078      | 43             | 37          | 0.33(5)     | 10.2 | 18.0                       |                    |                     |                       |  |  |
| hh)            | He             | 1.28            | 625            | 55                      | 1500             | 4.078      | 43             | 37          | 0.33(5)     | 10.2 | 18.0                       |                    |                     |                       |  |  |
| ii)            | He             | 1.28            | 625            | 55                      | 1500             | 4.078      | 43             | 37          | 0.33(5)     | 10.2 | 18.0                       |                    |                     |                       |  |  |
| jj)            | He             | 1.28            | 625            | 55                      | 1500             | 4.078      | 43             | 37          | 0.33(5)     | 10.2 | 18.0                       |                    |                     |                       |  |  |
| kk)            | He             | 1.28            | 625            | 55                      | 1500             | 4.078      | 43             | 37          | 0.33(5)     | 10.2 | 18.0                       |                    |                     |                       |  |  |
| ll)            | He             | 1.28            | 625            | 55                      | 1500             | 4.078      | 43             | 37          | 0.33(5)     | 10.2 | 18.0                       |                    |                     |                       |  |  |
| mm)            | He             | 1.28            | 625            | 55                      | 1500             | 4.078      | 43             | 37          | 0.33(5)     | 10.2 | 18.0                       |                    |                     |                       |  |  |
| nn)            | He             | 1.28            | 625            | 55                      | 1500             | 4.078      | 43             | 37          | 0.33(5)     | 10.2 | 18.0                       |                    |                     |                       |  |  |
| oo)            | He             | 1.28            | 625            | 55                      | 1500             | 4.078      | 43             | 37          | 0.33(5)     | 10.2 | 18.0                       |                    |                     |                       |  |  |
| pp)            | He             | 1.28            | 625            | 55                      | 1500             | 4.078      | 43             | 37          | 0.33(5)     | 10.2 | 18.0                       |                    |                     |                       |  |  |
| qq)            | He             | 1.28            | 625            | 55                      | 1500             | 4.078      | 43             | 37          | 0.33(5)     | 10.2 | 18.0                       |                    |                     |                       |  |  |
| rr)            | He             | 1.28            | 625            | 55                      | 1500             | 4.078      | 43             | 37          | 0.33(5)     | 10.2 | 18.0                       |                    |                     |                       |  |  |
| ss)            | He             | 1.28            | 625            | 55                      | 1500             | 4.078      | 43             | 37          | 0.33(5)     | 10.2 | 18.0                       |                    |                     |                       |  |  |
| tt)            | He             | 1.28            | 625            | 55                      | 1500             | 4.078      | 43             | 37          | 0.33(5)     | 10.2 | 18.0                       |                    |                     |                       |  |  |
| uu)            | He             | 1.28            | 625            | 55                      | 1500             | 4.078      | 43             | 37          | 0.33(5)     | 10.2 | 18.0                       |                    |                     |                       |  |  |
| vv)            | He             | 1.28            | 625            | 55                      | 1500             | 4.078      | 43             | 37          | 0.33(5)     | 10.2 | 18.0                       |                    |                     |                       |  |  |
| ww)            | He             | 1.28            | 625            | 55                      | 1500             | 4.078      | 43             | 37          | 0.33(5)     | 10.2 | 18.0                       |                    |                     |                       |  |  |
| xx)            | He             | 1.28            | 625            | 55                      | 1500             | 4.078      | 43</td         |             |             |      |                            |                    |                     |                       |  |  |

FIGURES

Fig. 6. A detailed comparison, peak by peak, of the observed and calculated Intensities plotted vs.  $S^2$  with Miller indices indicated (see Figs. 2, 5 and Table II).

Fig. 1. Schematic diagram of the metal cluster generator with TC - thermocouple, W - prism mirror window, H - heater for metal vaporization,  $S_1$  and  $S_2$  - sets of screws for configuration adjustments, CG-carrier gas,  $N_1$  and  $N_2$  - flow orifices or nozzles.

Fig. 2. Microdensitometer tracings of Experiments 16, 72 and 30 (see Table II). O.D. is the optical density,  $\log_{10}(I/I_0)$  and  $S = 4\pi\lambda^{-1}$  in  $(\theta/2)$ . Plate 30 is displaced 0.5 O.D. for clarity and Miller indices are shown.

Fig. 3. Experimental cluster size  $D_q$ , as a function of oven pressure and temperature determined using Eq. (2) for several metals and carrier gases.

Fig. 4. Theoretical diffracted intensities for fcc silver clusters, normalized to the  $\{311\}$  peak and plotted as a function of diameter  $D_t$ .

Fig. 5. The goodness of fit  $R_N$  worsens as size  $D_q$  decreases, indicating greater deviation from the fcc structure model. Points are labeled with the experiment numbers of Table II.

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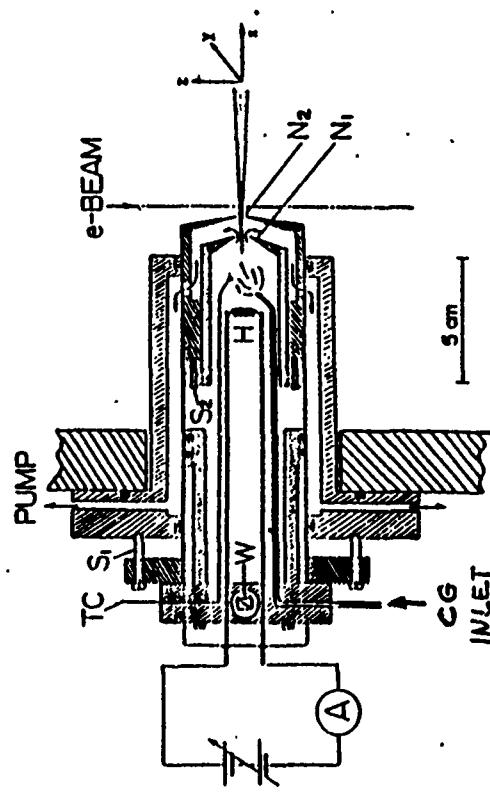
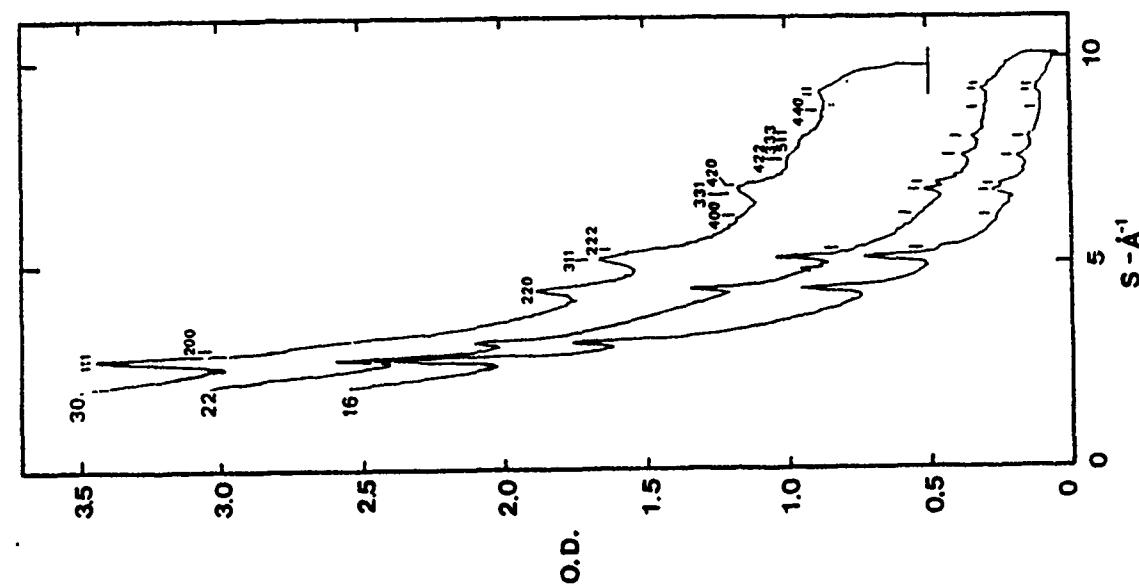


Figure 1

Figure 2



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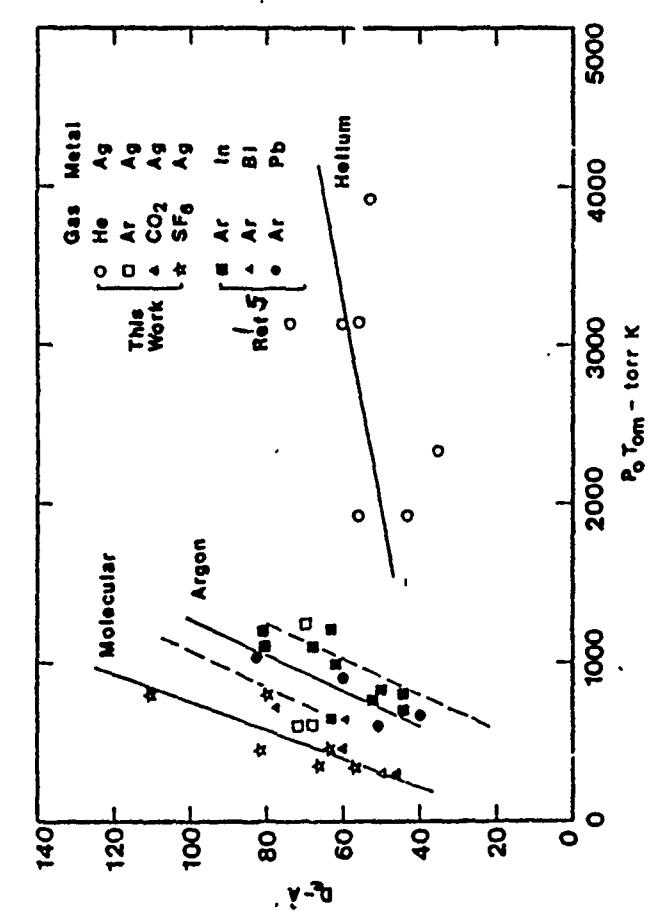


Figure 3

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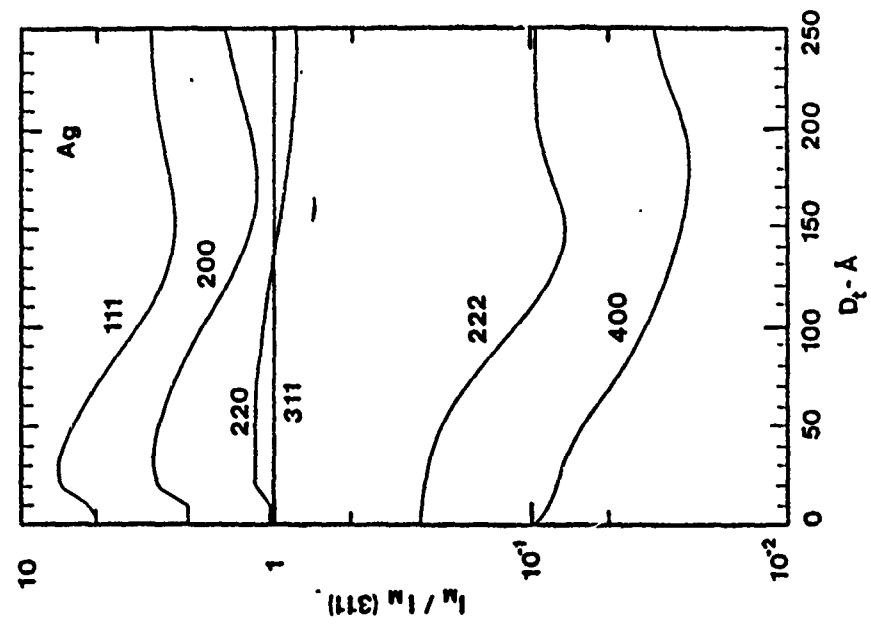


Figure 4

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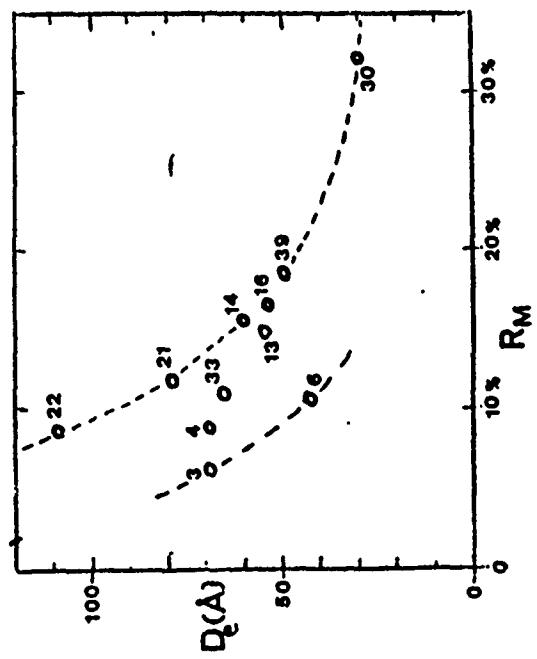


Figure 5

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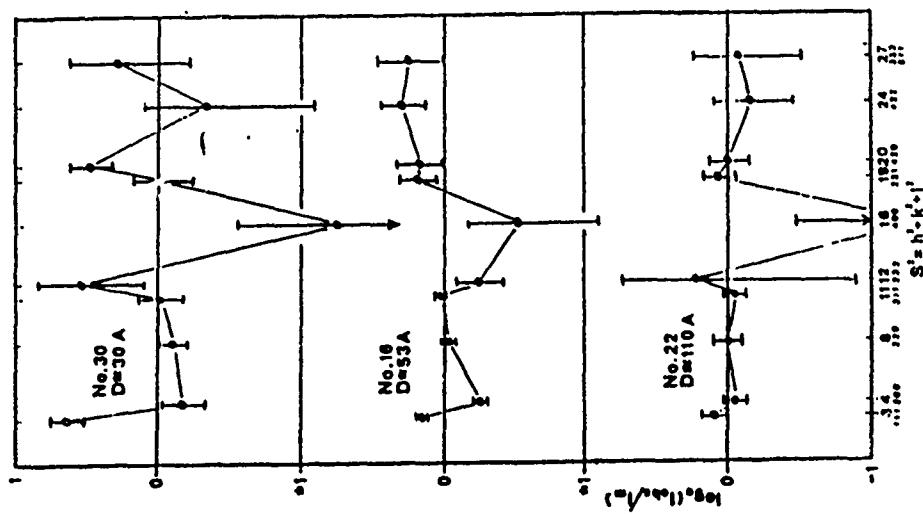


Figure 6